

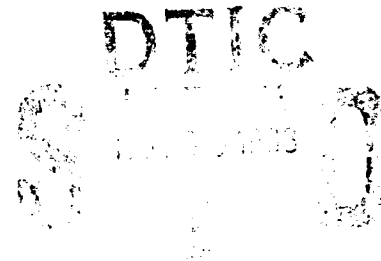


**US Army Corps
of Engineers**

Hydrologic Engineering Center



Application of the HEC Prescriptive Reservoir Model in the Columbia River System



Technical Paper No. 146

May 1993

Approved for Public Release. Distribution Unlimited.

93-29290



Papers in this series have resulted from technical activities of the Hydrologic Engineering Center. Versions of some of these have been published in technical journals or in conference proceedings. The purpose of this series is to make the information available for use in the Center's training program and for distribution within the Corps of Engineers

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.

Accession For	
NTIS CRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution	
Availability Codes	
Dist	Avail and/or Special
A-1	

DTIC QUALITY INSPECTED 3

Application of the HEC Prescriptive Reservoir Model In the Columbia River System

By Richard Hayes¹, Michael Burnham¹, and David Ford²

Abstract

The water resources of Columbia River system provide significant hydropower, water supply, flood control, recreation, fishery and navigation benefits to the residents of the Pacific Northwest. Increasingly, the competition among the users of the Columbia system has been intensified by declining fishery resources. The Corps of Engineers (Corps), U.S. Bureau of Reclamation (Reclamation) and Bonneville Power Administration (BPA) are jointly conducting a review of fourteen federal projects within the Columbia basin. This effort has been termed the Columbia River System Operation Review (SOR). To provide the Corps SOR study team with a basis for more optimal allocation of system resources, the Hydrologic Engineering Center (HEC) has applied the recently developed Prescriptive Reservoir Model, HEC-PRM, to the major reservoirs of the Columbia River system upstream of Bonneville Dam.

The HEC-PRM represents the Columbia system as a link-node network and uses network-flow programming to optimize, in time and space, flow and storage in the system. The representation of operational goals in HEC-PRM is accomplished through flow, storage and energy economic penalty functions. Operational purposes represented by penalty functions included hydropower, water supply, flood control, navigation, recreation, and anadromous fish. The application was based on fifty year period-of-record with a monthly time interval. The HEC data storage system, HEC-DSS, was utilized extensively for data management and analysis of results.

This paper summarizes the interim findings of the second phase of this ongoing application.

System Description

The Columbia River basin embraces approximately 259,000 sq. mi. (670,000 sq. km.) of the Pacific Northwest from Canadian Province of British Columbia in the north to

¹ Hydraulic Engineer and Chief of Planning, Respectively, US Army Corps of Engineers, Water Resources Support Center, Hydrologic Engineering Center, Davis, CA.

² Engineering Consultant, Sacramento, CA.

northern Nevada at its most southern point, and from the Pacific Ocean on the west to Wyoming on the east. Major storage and run-of-river reservoirs on the Columbia and its major tributaries (the Kootenai, Pend Oreille, Snake and Clearwater Rivers) are shown in Figure 1.

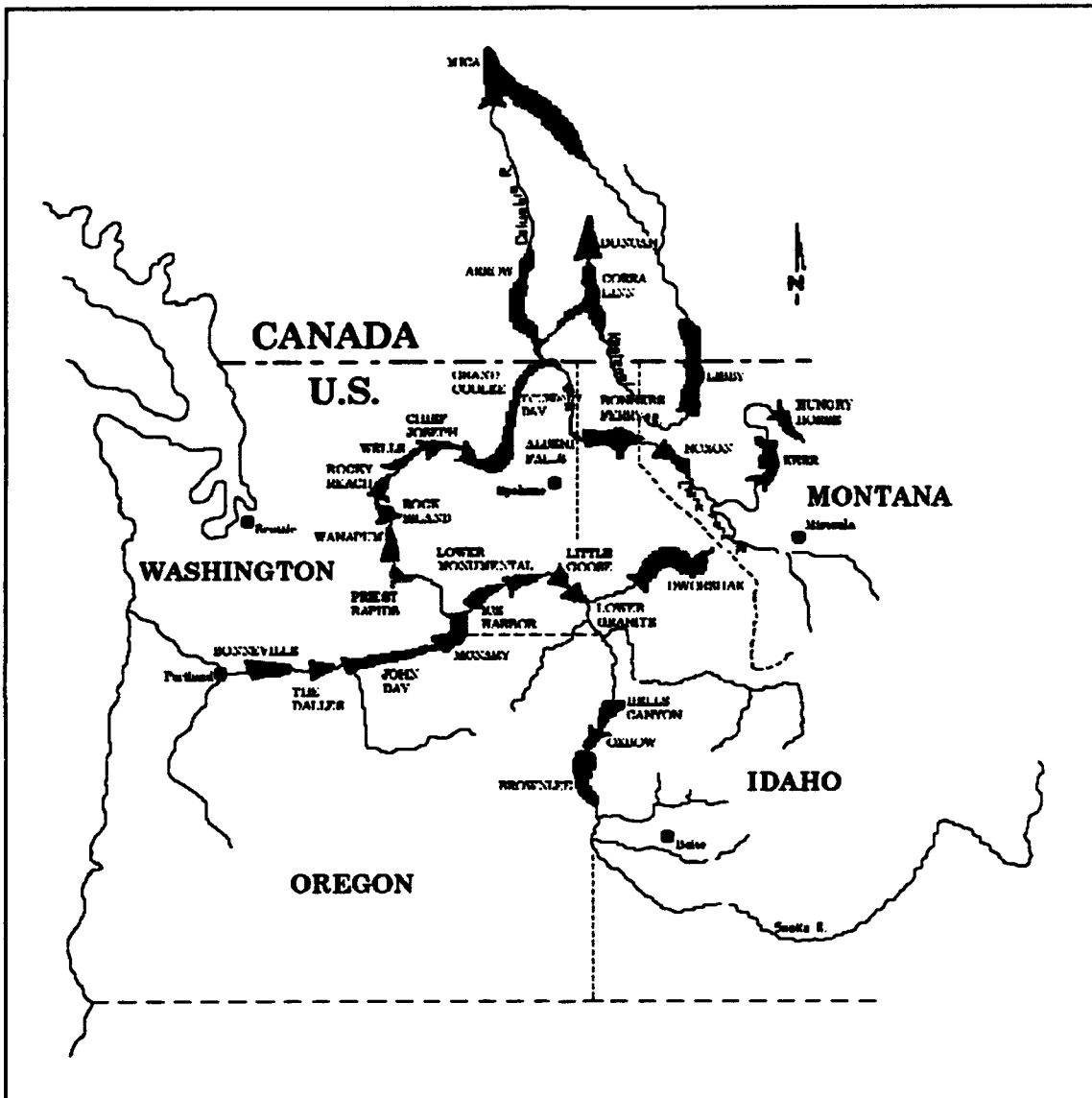


Figure 1 Columbia River System

Average annual runoff is about 275,000 cfs (7,790 cms), of which 25 percent comes from Canada. Precipitation varies from an annual total of over 100 inches near Mica in British Columbia and along Cascade Range at the basin's western boundary to about 6 inches in southern Idaho and central Washington. Runoff from the basin above Bonneville Dam has a strong seasonal pattern with most runoff resulting from snowmelt in April through July.

Water Resources Development

Development of federal reservoirs along the main stem of the Columbia began in the 1930's primarily as consequence of nationwide unemployment during the Great Depression. Bonneville, a Corps navigation and hydropower project, was begun by the Works Progress Administration and was completed by the Corps in 1938. Grand Coulee, Reclamation's mainstem Columbia irrigation and hydropower project, went in service in 1941. Energy from both projects contributed significantly to the regions rapid industrial growth during World War II.

During the 1950's the Corps completed The Dalles, McNary, and Chief Joseph on the Columbia and Albeni Falls on the Pend Oreille River. Reclamation added Hungry Horse Reservoir on the Flathead River to the federal system in 1952. During the 1960's the Corps continued development of the Columbia-Snake River Waterway navigation system by finishing John Day on the Columbia and Ice Harbor and Lower Monumental on the lower Snake River. Corps development in the Snake River basin continued in the 1970's with Little Goose and Lower Granite on the Snake River and Dworshak on the North Fork of Clearwater River.

In January 1961, the United States and Canada became signatories to the Columbia River Treaty. The treaty provided for cooperative development of four storage projects to be operated for flood control and hydropower: Libby in Montana; and Mica, Arrow, and Duncan in British Columbia. Duncan, the first of the Canadian Treaty projects was completed in 1967; Arrow (Hugh Keenleyside) was completed in 1968; and, Mica was completed in 1973. In 1975, the Corps completed Libby Dam, the fourteenth federal reservoir included in the ongoing System Operation Review (SOR) investigations.

In addition to the major federal and treaty projects, numerous other reservoirs have been developed throughout the system principally for hydropower and irrigation. The Columbia River Basin Master Water Control Manual (USACE, 1984) indicates that the Columbia Basin above its mouth includes 211 water control projects with a storage greater than 5,000 acre-feet or installed capacity of 5 mW or more.

The Problem

While reservoir projects within the Columbia Basin have provided significant flood control, irrigation, hydropower, recreation and navigation benefits for the region the cumulative effect of these works coupled with pollution, over harvesting, and other habitat changes have had an impact on the Columbia River fishery. According to the Master Water Control Manual, the 1911 harvest of Columbia River salmon and steelhead was about 50 million pounds. This figure has been estimated to be approximately the natural sustainable annual yield. The 1911 harvest stands in sharp contrast to the 10 million pound harvest in 1989 cited in The Columbia River System: The Inside Story (Interagency Team, 1991). The federal agencies and the fish and wildlife departments of Idaho,

Oregon and Washington have invested heavily in physical facilities including fish hatcheries, ladders, screens and bypass facilities.

Operation modifications to aid the downstream migration of juvenile salmon and steelhead including provisions for increased springtime flows and spillway discharges are being utilized. Still other operation alternatives involving seasonal storage drawdowns, primarily on the navigation impoundments of the lower Snake River and increased flows from upstream storage reservoirs have been proposed. Operational or physical modifications to meet changing demands or enhance any of the uses at the various reservoirs and stream reaches of Columbia River will in all likelihood impact to some degree one or more of the other system uses.

The problems of operating the coordinated system of flood control and hydropower reservoirs by BPA, the Corps, and Reclamation are summarized in *The Columbia River: A System Under Stress* (BPA, USACE, BuRec, 1990) in which they state:

Growth in our region, along with changing priorities, are putting our river system increasingly under stress. There simply is not enough water flowing in the system to meet all the demands. Trade-off must be considered ... in recent years, demands by the various users of the river have increased dramatically, resulting in increasing conflicts among uses.

Consequently, in 1990 the North Pacific Division (NPD) of the Corps of Engineers proposed the interagency system operation review. To assist in the evaluation of the system and the analysis of potential trade-offs NPD requested the Hydrologic Engineering Center to provide technical assistance in the further development and application of the Center's reservoir system optimization model, HEC-PRM.

HEC-PRM

The HEC has recently developed a prescriptive reservoir model to assist in the analysis of Corps reservoir systems. This new model has been termed HEC-PRM (USACE, 1991a). The term "prescriptive" may be explained in part by comparison with the characteristics of another HEC reservoir system model, the widely applied HEC-5 (USACE, 1982a). HEC-5 is classified as a "descriptive" reservoir model. Both types of models are similar in that they require a sequence of flows and link-node descriptions for continuity of flow. In a descriptive model, like HEC-5, operation policies are specified as storage rule curves, channel capacities, hydropower energy demands, diversions and flow requirements. The outcome of an HEC-5 simulation is typically a time series of flows, stages, and energy production which is obtained by following a specified operation policy. The evaluation of specified operation policies to select the "optimal" among those simulated is left to the model user.

HEC-PRM, on the other hand, uses as a formal objective function the minimization of total system cost. The model uses a network flow solver developed by Jensen and Bhaumik (1974) to determine the optimal distribution of flow, storage and energy production in space and time. The primary input to the HEC-PRM model are "penalty" functions, which relate the consequence (cost) of flow, storage and energy production in a system, and a network description to provide the basis for continuity as flow moves through a system of links and nodes. The penalty functions provide an economic basis for operation prioritization. The model automatically nominates alternative policies which it evaluates with a built-in simulation module. Feasible alternatives are evaluated until a minimum cost policy is determined.

For convenience, HEC-PRM input penalty functions and flow sequences, as well as optimized flows and storages, are handled with HEC-DSS (USACE, 1990). The HEC-DSS utility programs DSSMATH, DSSUTL and DDISPLAY are used to develop, manage and plot time series data. Two HEC-PRM utility programs PENF (a graphical penalty function editor) and PRMPP (a post processor) are currently being developed and tested.

Columbia River HEC-PRM Application

HEC-PRM was demonstrated to be an appropriate tool for the analysis of reservoirs with its first application on the Missouri River system. This application for the Corps Missouri River Division (MRD) on the Corps' six mainstem reservoirs was completed in 1990 (USACE, 1991b). The Missouri River system, from the stand point of system optimization, is a relatively straight foreword system with six large tandem reservoirs under the same management. The competing interests in the Missouri system included lake recreation, hydropower production, flood control, water supply and downstream navigation and environmental concerns.

The Corps North Pacific Division (NPD) in 1990 proposed an interagency review of the Columbia River system. The Columbia River, like the Missouri, has recently experienced a system wide water shortage that exacerbated the competition among the various system users. The two systems are similar in that they both have almost the same types of competing interests. The principle exception being in the Missouri system the major environmental concern is maintenance of steady flows for sand bar nesting birds; whereas, the major environmental concern of the Columbia system is the maintenance of seasonal flows to aid the downstream migration salmon and steelhead.

The NPD, as a part of the SOR requested HEC to test the applicability of HEC-PRM to the more complex and larger Columbia River system. This effort, termed Phase I, was initiated in and completed in 1991. It was anticipated that a second phase would follow with more economic detail if the Phase I application proved successful. The findings of the Phase I of the application are reported in Columbia River System Analysis Model - Phase I (USACE, 1991b). The results of the Phase I application verified the applicability of HEC-PRM to a complex system such as the Columbia. It was determined

that the HEC would proceed with the second phase of the analysis. It was agreed that this effort would include the following: expansion of the network to include more storage reservoirs; enhancements to the HEC-PRM hydropower analysis capability; analysis of several alternatives; and a workshop to transfer the technology the Corps SOR team.

HEC began the second phase of the application in fall of 1991. The Phase II network configuration is shown in Figure 2. The network includes fourteen storage reservoirs, five run-of-river (pondage) reservoirs and three non-reservoir locations.

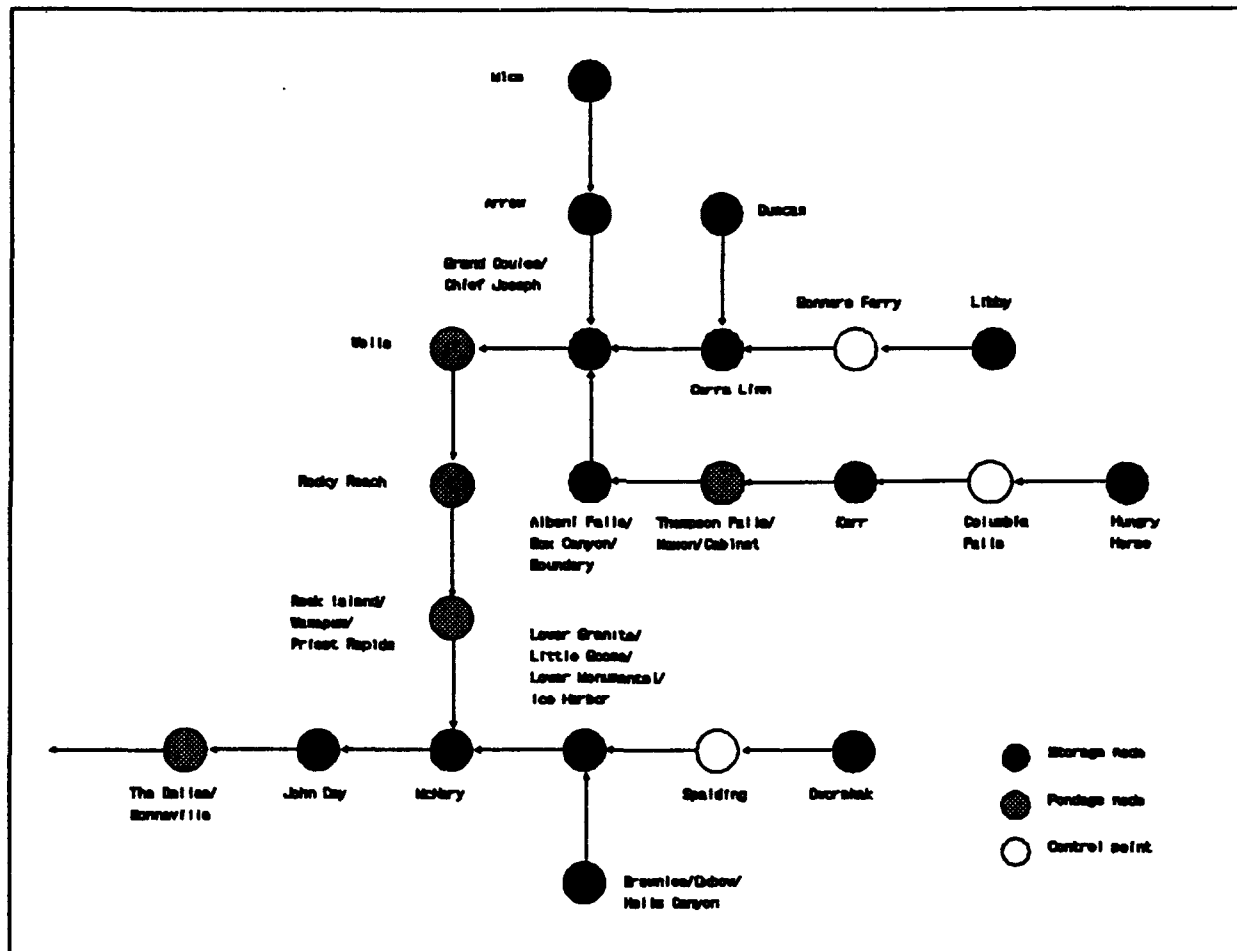


Figure 2 Single-period Network Model of Columbia River System

During the Phase I application it was noted that HEC-PRM storages for Corra Linn (Lake Kootenay), a Canadian hydropower project on the Kootenay River, did not correspond to the simulation results of NPD's HYSSR (USACE, 1982b) simulation model to the degree deemed reasonable. Upon investigation it was determined that Corra Linn did not have sufficient outlet capacity to prevent storage from exceeding upper storage

limit. It was further determined that two other reservoirs in the system could also exhibit the same characteristic. The other two are Kerr (Flathead Lake) and Albeni Falls (Lake Pend Oreille). All three are similar in that they are control structures located on a river reach some distance from a natural lake. In order to model these reservoirs, the nominal upper storage was raised to an arbitrarily high value and a restrictive maximum flow limit was specified. To discourage HEC-PRM from utilizing this zone in other than a flood condition, the reservoir storage penalties were modified to inflict a relatively high cost for storage above the nominal full pool. The results obtained have been determined to be appropriate for the current application. It is anticipated that policies determined with HEC-PRM will be modeled with a simulation model, in this case HYSSR, which can provide the additional operational details. Reservoir storage and flow limits are shown in Table 1.

Table 1
Columbia River System Storage and Release Limits

<u>Reservoir</u>	<u>Storage Limits, 1000 Acre-Feet</u>		<u>Release Limits - CFS</u>	
	<u>Minimum</u>	<u>Maximum</u>	<u>Minimum</u>	<u>Maximum</u>
Libby	889.9	5,869.4	3,000	—
Corra Linn	144.0	9,999.0	—	55,940
Duncan	30.0	1,398.6	100	—
Hungry Horse	486.0	3,647.1	400	—
Kerr	572.3	9,999.0	1,500	54,930
Albeni Falls	446.4	9,999.0	—	129,800
Dworshak	1,452.2	3,468.0	1,000	—
Brownlee	431.7	1,426.7	5,000	—
Granite	144.0	1,825.0	—	—
Mica (Alts. 1 & 2)	13,075.0	20,075.0		
Mica (Alt. 3)	8,000.0	20,075.0		
Arrow	227.0	7,327.0	5,000	—
Grand Coulee	3,879.0	9,107.4	—	—
McNary	1,170.0	1,350.0	—	—
John Day	1,989.0	2,523.0	—	—

Penalty functions are the "guiding light" with which HEC-PRM determines the optimal distribution of flow and storage in time and space. For the Columbia River application, penalty functions represented the following six types of system uses: hydropower; flood control; navigation; anadromous fish; water supply; and, recreation.

The hydropower penalty function is expressed in terms of both flow and variable storage. Each of the other uses were expressed in terms of a flow penalty in \$/kaf (1,000's acre feet per month) or a storage penalty in \$/kaf. Penalty functions are varied monthly to reflect the seasonal nature of the various purposes. At each location, the various penalty functions are combined to create a composite function for each month. HEC-PRM requires that all penalties must be piecewise linear convex functions. Figure 3 shows how penalty functions are combined and how an approximate edited function is determined to satisfy the convex requirement.

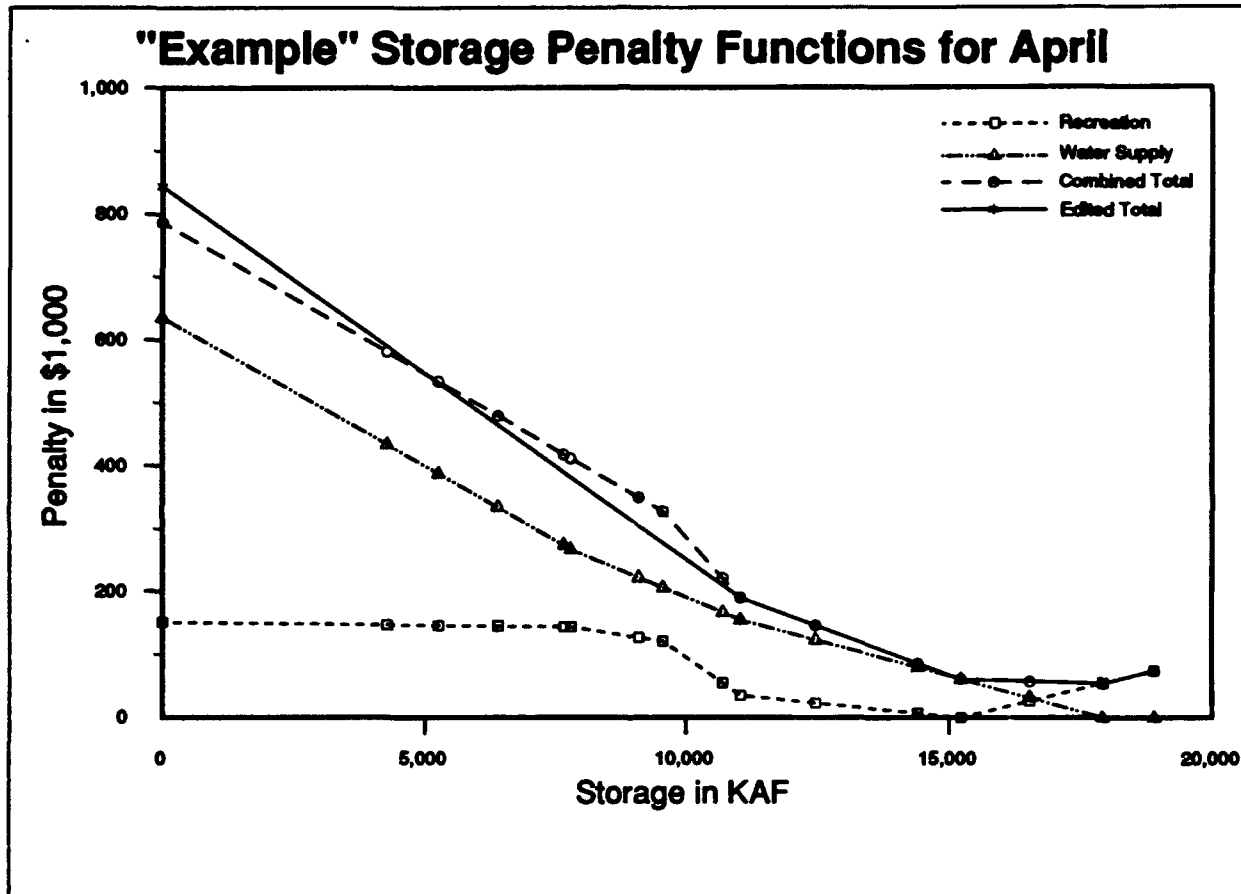


Figure 3 How Penalty Functions are Combined and Approximated

Economic data to create the necessary penalty functions was developed by Corps economists, planners, and engineers from NPD and the Division's Seattle, Portland and Walla Walla Districts under the direction of the Corps Institute for Water Resources (IWR). These data are documented in "Economic Value Functions for Columbia River System Analysis Model, Phase I (Draft)", (USACE, 1992). A graphical penalty function editor (PENF), which was developed during this phase, was used to develop the edited penalty functions. Economic data to develop penalty functions for the Canadian Treaty

reservoirs (Mica, Arrow and Duncan) were not available for use in this phase. Table 2 indicates the purposes which were represented by economic penalty functions throughout the network.

Analysis Overview

The operation for the system was based on flows for the period of 1928 to 1978. Monthly flow data for this period, adjusted to a consistent level of development (1980) were provided by NPD (USACE, 1983). Irrigation depletions, returns and reservoir evaporation were accounted for in the flow data. Irrigation withdrawals from Grand Coulee to Bureau of Reclamation's Columbia Basin Project were treated as a fixed diversion (e.g. not optimized). Three system operation scenarios were selected for analysis, they were: Alternative 1, existing storage allocations with optimization for all operation purposes; Alternative 2, existing storage allocations without optimization for hydropower; and Alternative 3, five million acre-feet of additional storage in Mica, optimization for all operation purposes.

To evaluate system performance of all alternatives with a consistent frame of reference, which represented the present system with current rules and objectives, the results of NPD's continuous HYSSR simulation (SOR base case) were utilized. To provide a valid economic comparison, HYSSR flows and storages were applied to HEC-PRM storage, flow and hydropower penalty functions.

The analyses were performed on a 25 mHz 80486 MS-DOS personal computer with 16 mb memory. The current version of HEC-PRM utilizes allocatable arrays and virtual memory management, which make it extremely accommodating from a users point of view. Execution times for Alternatives 1 and 3 (about 150,000 simultaneous linear equations) for the 50 years of record were about fourteen hours each. For alternative 2, which did not optimize for hydropower, about three hours of execution time was required. Analyses for shorter time spans took significantly less execution time. It is worthwhile to note that for the Columbia system, which has a relatively small amount of storage compared to the annual flow, the presumed requirement to run the entire period of record in a single optimization run is not valid. The analyst has merely to start and end the optimization period at times when the system would be reliably full, which, in the case of the Columbia system, is frequently the case at the end of spring runoff.

To compare the analyses results, performance of all three alternatives and the HYSSR simulation have been computed with the following indices: total system penalty (as computed with HEC-PRM); reliability (the frequency of meeting monthly targets); resiliency (the frequency of recovery after a failure); and vulnerability (the average deviation from the target when a failure occurs).

Table 2
Columbia River System Phase II Network Links and Operation Purposes Penalty Functions

Original Node ¹ (1)	Terminal Node ¹ (2)	Link Type ² (3)	Operation purposes modeled ³					
			FC (4)	Hydro (5)	Nav (6)	Irr/WS (7)	Fish (8)	Rec (9)
Libby	Libby	S						✓
Libby	Bonniers Ferry	H		✓				✓
Bonniers Ferry	Corra Linn	C	✓					
Duncan	Duncan	S						
Duncan	Corra Linn	R	✓					
Corra Linn	Corra Linn	S	✓					
Corra Linn	Coulee	R						
Hungry Horse	Hungry Horse	S						✓
Hungry Horse	Columbia Falls	H		✓				
Columbia Falls	Kerr	C	✓					
Kerr	Kerr	S	✓					
Kerr	Thompson	H	✓	✓				
Thompson	Thompson	S						
Thompson	Albeni	H		✓				
Albeni	Albeni	S	✓					✓
Albeni	Coulee	H	✓	✓				
Dworshak	Dworshak	S			✓			✓
Dworshak	Spalding	H		✓				
Spalding	Granite	C	✓					
Brownlee	Brownlee	S						
Brownlee	Granite	H		✓				
Granite	Granite	S			✓	✓		✓
Granite	McNary	H		✓			✓	
Mica	Mica	S						
Mica	Arrow	R						
Arrow	Arrow	S						
Arrow	Coulee	R						
Coulee	Coulee	S				✓		✓
Coulee	Wells	H		✓				
Wells	Wells	S						
Wells	Rocky Reach	H		✓				
Rocky Reach	Rocky Reach	S						
Rocky Reach	Rock Island	H		✓				
Rock Island	Rock Island	S						
Rock Island	McNary	H		✓				
McNary	McNary	S			✓	✓		✓
McNary	John Day	H		✓				
John Day	John Day	S			✓	✓		
John Day	Dalles	H		✓				
Dalles	Dalles	S						
Dalles	Sink	H	✓	✓			✓	

¹ Refer to Figure 2 for relative location of nodes.

² R = simple reservoir-release link; S = storage (period to period) link; H = hydropower reservoir-release link; C = channel-flow link; D = diversion link.

³ FC = flood control; Hydro = hydroelectric-power generation; Nav = navigation; Irr/WS = irrigation and/or water supply; Fish = fish protection; Rec = recreation.

Optimization results contrasting the three alternatives with HYSSR results at Dworshak Reservoir (storage) and The Dalles (flow) are shown in Figures 4 and 5 respectively, for the period of 1928-1938.

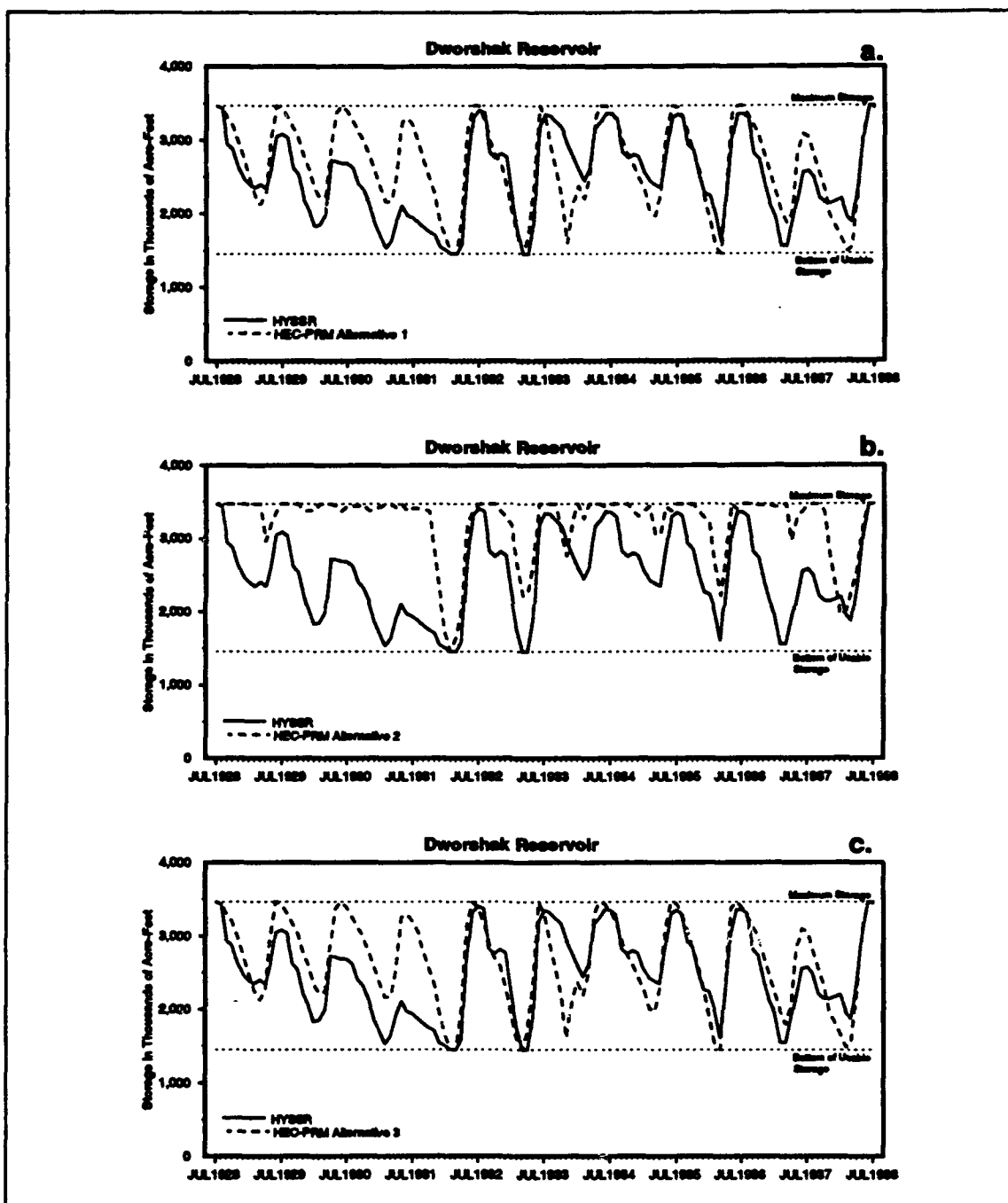


Figure 4 1928-1938 Storage at Dworshak: HYSSR & Alternatives

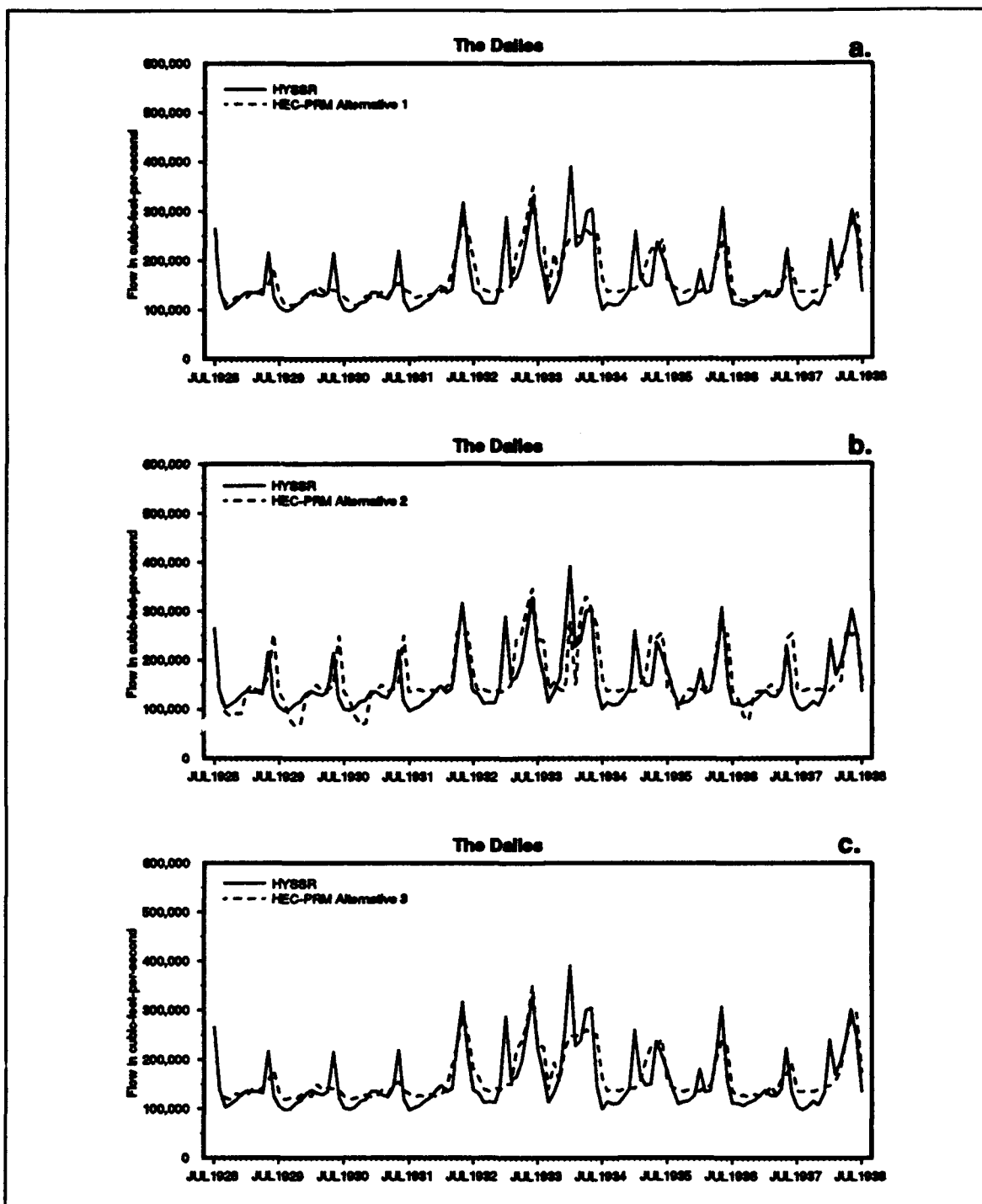


Figure 5 1928-1938 Flow at The Dalles: HYSSR & Alternatives

Study Status

A draft report, Columbia River Reservoir System Analysis: Interim Findings, (Draft), April 1993 has been transmitted to the North Pacific Division for review. It is anticipated that a workshop to transfer the HEC-PRM model and the input files that were developed in this study will be presented to Corps SOR team members in July 1993. At the time of the workshop, it is expected that economic data to develop penalty functions for the Canadian treaty reservoirs may become available. Additional work will be required to develop reservoir operating rules which closely follow the optimal time series of storage and flow, HEC hopes to assist NPD in this effort. The HEC will publish a Phase II report at the conclusion of the study. HEC plans to make a version of HEC-PRM available to the public by the middle of 1993.

Conclusion and Observations

1. HEC-PRM has been demonstrated to be capable of period-of-record optimization of complex systems of reservoirs with commonly available computer systems.
2. The partially updated Phase I economic data which was the basis for this study should be revisited.
3. Penalty data for the Canadian Treaty reservoirs should be developed.

Acknowledgements

This project was supported by the U.S. Army Corps of Engineers, North Pacific Division and Corps research funds. Dr. David Moser of the Institute for Water Resources guided the development of the economic penalty functions. Dr. Quentin Martin, of the Lower Colorado River Authority, played a key role in the implementation and testing of the HEC-PRM hydropower algorithm. Vladamir Plesa, of the University of California, Davis, developed the PENF and PRMPP programs during the study. Robert Carl, of the Hydrologic Engineering Center (HEC), developed the HEC-PRM computer software, contributed to overall analysis and generated the post processing results. Marilyn Hurst, of HEC, performed data preparation, and analysis of results. Loshan Law, of HEC, typed and assembled the report. Darryl Davis, HEC Director, provided general supervision and guidance for the project.

References

BPA, USACE, BuRec, (1990). *The Columbia river: A system under stress*. Portland, OR.

Interagency Team, (1991), *The Columbia River System: The Inside Story*, USACE, Portland, OR.

Jensen, P.A., Bhaumik, G., and Driscoll, B., (1974). "Network flow modeling of multireservoir water distribution systems," *CRWR-107*, University of Texas, Austin, TX.

U.S. Army Corps of Engineers, (1982a), *HEC-5: Simulation of Flood Control and Conservation Systems, User's Manual*. Hydrologic Engineering Center, Davis CA.

U.S. Army Corps of Engineers, (1982b), *HYSSR (Hydro System Seasonal Regulation), Program Users Manual*. North Pacific Division, Portland OR.

U.S. Army Corps of Engineers, (1983), *1980 Level Modified Streamflow, 1828-1978, Columbia River and Coastal Basins*. Depletions Task Force, Columbia River Water Management Group, Portland OR.

U.S. Army Corps of Engineers, (1984), *Columbia River Basin, Master Water Control Manual*. North Pacific Division, Portland OR.

U.S. Army Corps of Engineers, (1990), *HEC-DSS User's Guide and Utility Program Manuals*. Hydrologic Engineering Center, Davis CA.

U.S. Army Corps of Engineers, (1991a), *HECPRM, Hydrologic Engineering Center's Prescriptive Reservoir Model, Program Description*, Hydrologic Engineering Center, Davis, CA.

U.S. Army Corps of Engineers, (1991b), *Columbia River System Analysis Model - Phase I*. Hydrologic Engineering Center, Davis CA.

U.S. Army Corps of Engineers, (1992), *Economic Value Functions for Columbia River System Analysis Model (Draft)*. Institute for Water Resources, Fort Belvoir, VA.

TECHNICAL PAPER SERIES **(\$2 per paper)**

TP-1	Use of Interrelated Records to Simulate Streamflow	TP-38	Water Quality Evaluation of Aquatic Systems
TP-2	Optimization Techniques for Hydrologic Engineering	TP-39	A Method for Analyzing Effects of Dam Failures in Design Studies
TP-3	Methods of Determination of Safe Yield and Compensation Water from Storage Reservoirs	TP-40	Storm Drainage and Urban Region Flood Control Planning
TP-4	Functional Evaluation of a Water Resources System	TP-41	HEC-5C, A Simulation Model for System Formulation and Evaluation
TP-5	Streamflow Synthesis for Ungaged Rivers	TP-42	Optimal Sizing of Urban Flood Control Systems
TP-6	Simulation of Daily Streamflow	TP-43	Hydrologic and Economic Simulation of Flood Control Aspects of Water Resources Systems
TP-7	Pilot Study for Storage Requirements for Low Flow Augmentation	TP-44	Sizing Flood Control Reservoir Systems by Systems Analysis
TP-8	Worth of Streamflow Data for Project Design - A Pilot Study	TP-45	Techniques for Real-Time Operation of Flood Control Reservoirs in the Merrimack River Basin
TP-9	Economic Evaluation of Reservoir System Accomplishments	TP-46	Spatial Data Analysis of Nonstructural Measures
TP-10	Hydrologic Simulation in Water-Yield Analysis	TP-47	Comprehensive Flood Plain Studies Using Spatial Data Management Techniques
TP-11	Survey of Programs for Water Surface Profiles	TP-48	Direct Runoff Hydrograph Parameters Versus Urbanization
TP-12	Hypothetical Flood Computation for a Stream System	TP-49	Experience of HEC in Disseminating Information on Hydrological Models
TP-13	Maximum Utilization of Scarce Data in Hydrologic Design	TP-50	Effects of Dam Removal: An Approach to Sedimentation
TP-14	Techniques for Evaluating Long-Term Reservoir Yields	TP-51	Design of Flood Control Improvements by Systems Analysis: A Case Study
TP-15	Hydrostatistics - Principles of Application	TP-52	Potential Use of Digital Computer Ground Water Models
TP-16	A Hydrologic Water Resource System Modeling Techniques	TP-53	Development of Generalized Free Surface Flow Models Using Finite Element Techniques
TP-17	Hydrologic Engineering Techniques for Regional Water Resources Planning	TP-54	Adjustment of Peak Discharge Rates for Urbanization
TP-18	Estimating Monthly Streamflows Within a Region	TP-55	The Development and Servicing of Spatial Data Management Techniques in the Corps of Engineers
TP-19	Suspended Sediment Discharge in Streams	TP-56	Experiences of the Hydrologic Engineering Center in Maintaining Widely Used Hydrologic and Water Resource Computer Models
TP-20	Computer Determination of Flow Through Bridges	TP-57	Flood Damage Assessments Using Spatial Data Management Techniques
TP-21	An Approach to Reservoir Temperature Analysis	TP-58	A Model for Evaluating Runoff-Quality in Metropolitan Master Planning
TP-22	A Finite Difference Method for Analyzing Liquid Flow in Variably Saturated Porous Media	TP-59	Testing of Several Runoff Models on an Urban Watershed
TP-23	Uses of Simulation in River Basin Planning	TP-60	Operational Simulation of a Reservoir System with Pumped Storage
TP-24	Hydroelectric Power Analysis in Reservoir Systems	TP-61	Technical Factors in Small Hydropower Planning
TP-25	Status of Water Resource Systems Analysis	TP-62	Flood Hydrograph and Peak Flow Frequency Analysis
TP-26	System Relationships for Panama Canal Water Supply	TP-63	HEC Contribution to Reservoir System Operation
TP-27	System Analysis of the Panama Canal Water Supply	TP-64	Determining Peak-Discharge Frequencies in an Urbanizing Watershed: A Case Study
TP-28	Digital Simulation of an Existing Water Resources System	TP-65	Feasibility Analysis in Small Hydropower Planning
TP-29	Computer Applications in Continuing Education	TP-66	Reservoir Storage Determination by Computer Simulation of Flood Control and Conservation Systems
TP-30	Drought Severity and Water Supply Dependability	TP-67	Hydrologic Land Use Classification Using LANDSAT
TP-31	Development of System Operation Rules for an Existing System by Simulation	TP-68	Interactive Nonstructural Flood-Control Planning
TP-32	Alternative Approaches to Water Resource System Simulation	TP-69	Critical Water Surface by Minimum Specific Energy Using the Parabolic Method
TP-33	System Simulation for Integrated Use of Hydroelectric and Thermal Power Generation	TP-70	Corps of Engineers Experience with Automatic Calibration of a Precipitation-Runoff Model
TP-34	Optimizing Flood Control Allocation for a Multipurpose Reservoir	TP-71	Determination of Land Use from Satellite Imagery for Input to Hydrologic Models
TP-35	Computer Models for Rainfall-Runoff and River Hydraulic Analysis	TP-72	Application of the Finite Element Method to Vertically Stratified Hydrodynamic Flow and Water Quality
TP-36	Evaluation of Drought Effects at Lake Atitlan		
TP-37	Downstream Effects of the Levee Overtopping at Wilkes-Barre, PA, During Tropical Storm Agnes		

- TP-73 Flood Mitigation Planning Using HEC-SAM
TP-74 Hydrographs by Single Linear Reservoir Model
TP-75 HEC Activities in Reservoir Analysis
TP-76 Institutional Support of Water Resource Models
TP-77 Investigation of Soil Conservation Service Urban Hydrology Techniques
TP-78 Potential for Increasing the Output of Existing Hydroelectric Plants
TP-79 Potential Energy and Capacity Gains from Flood Control Storage Reallocation at Existing U. S. Hydropower Reservoirs
TP-80 Use of Non-Sequential Techniques in the Analysis of Power Potential at Storage Projects
TP-81 Data Management Systems for Water Resources Planning
TP-82 The New HEC-1 Flood Hydrograph Package
TP-83 River and Reservoir Systems Water Quality Modeling Capability
TP-84 Generalized Real-Time Flood Control System Model
TP-85 Operation Policy Analysis: Sam Rayburn Reservoir
TP-86 Training the Practitioner: The Hydrologic Engineering Center Program
TP-87 Documentation Needs for Water Resources Models
TP-88 Reservoir System Regulation for Water Quality Control
TP-89 A Software System to Aid in Making Real-Time Water Control Decisions
TP-90 Calibration, Verification and Application of a Two-Dimensional Flow Model
TP-91 HEC Software Development and Support
TP-92 Hydrologic Engineering Center Planning Models
TP-93 Flood Routing Through a Flat, Complex Flood Plain Using a One-Dimensional Unsteady Flow Computer Program
TP-94 Dredged-Material Disposal Management Model
TP-95 Infiltration and Soil Moisture Redistribution in HEC-1
TP-96 The Hydrologic Engineering Center Experience in Nonstructural Planning
TP-97 Prediction of the Effects of a Flood Control Project on a Meandering Stream
TP-98 Evolution in Computer Programs Causes Evolution in Training Needs: The Hydrologic Engineering Center Experience
TP-99 Reservoir System Analysis for Water Quality
TP-100 Probable Maximum Flood Estimation - Eastern United States
TP-101 Use of Computer Program HEC-5 for Water Supply Analysis
TP-102 Role of Calibration in the Application of HEC-6
TP-103 Engineering and Economic Considerations in Formulating
TP-104 Modeling Water Resources Systems for Water Quality
TP-105 Use of a Two-Dimensional Flow Model to Quantify Aquatic Habitat
TP-106 Flood-Runoff Forecasting with HEC-1F
TP-107 Dredged-Material Disposal System Capacity Expansion
TP-108 Role of Small Computers in Two-Dimensional Flow Modeling
TP-109 One-Dimensional Model For Mud Flows
TP-110 Subdivision Froude Number
TP-111 HEC-5Q: System Water Quality Modeling
TP-112 New Developments in HEC Programs for Flood Control
TP-113 Modeling and Managing Water Resource Systems for Water Quality
TP-114 Accuracy of Computed Water Surface Profiles - Executive Summary
TP-115 Application of Spatial-Data Management Techniques in Corps Planning
TP-116 The HEC's Activities in Watershed Modeling
TP-117 HEC-1 and HEC-2 Applications on the MicroComputer
TP-118 Real-Time Snow Simulation Model for the Monongahela River Basin
TP-119 Multi-Purpose, Multi-Reservoir Simulation on a PC
TP-120 Technology Transfer of Corps' Hydrologic Models
TP-121 Development, Calibration and Application of Runoff Forecasting Models for the Allegheny River Basin
TP-122 The Estimation of Rainfall for Flood Forecasting Using Radar and Rain Gage Data
TP-123 Developing and Managing a Comprehensive Reservoir Analysis Model
TP-124 Review of the U.S. Army Corps of Engineering Involvement With Alluvial Fan Flooding Problems
TP-125 An Integrated Software Package for Flood Damage Analysis
TP-126 The Value and Depreciation of Existing Facilities: The Case of Reservoirs
TP-127 Floodplain-Management Plan Enumeration
TP-128 Two-Dimensional Floodplain Modeling
TP-129 Status and New Capabilities of Computer Program HEC-6: "Scour and Deposition in Rivers and Reservoirs"
TP-130 Estimating Sediment Delivery and Yield on Alluvial Fans
TP-131 Hydrologic Aspects of Flood Warning - Preparedness Programs
TP-132 Twenty-five Years of Developing, Distributing, and Supporting Hydrologic Engineering Computer Programs
TP-133 Predicting Deposition Patterns in Small Basins
TP-134 Annual Extreme Lake Elevations by Total Probability Theorem
TP-135 A Muskingum-Cunge Channel Flow Routing Method for Drainage Networks
TP-136 Prescriptive Reservoir System Analysis Model - Missouri River System Application
TP-137 A Generalized Simulation Model for Reservoir System Analysis
TP-138 The HEC NexGen Software Development Project
TP-139 Issues for Applications Developers
TP-140 HEC-RAS/HEC-2 Comparison Study
TP-141 HEC-RAS Conveyance Comparison
TP-142 Systems Analysis Applications at the Hydrologic Engineering Center
TP-143 Runoff Prediction Uncertainty for Ungauged Agricultural Watersheds
TP-144 Review of GIS Applications in Hydrologic Modeling
TP-145 Application of Rainfall-Runoff Simulation for Flood Forecasting
TP-146 Application of the HEC Prescriptive Reservoir Model in the Columbia River System

REPORT DOCUMENTATION PAGE

Form Approved
 OMB No. 0704-0188

1a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED			1b. RESTRICTIVE MARKINGS		
2a. SECURITY CLASSIFICATION AUTHORITY			3. DISTRIBUTION / AVAILABILITY OF REPORT		
2b. DECLASSIFICATION / DOWNGRADING SCHEDULE					
4. PERFORMING ORGANIZATION REPORT NUMBER(S) * TECHNICAL PAPER NO. 146			5. MONITORING ORGANIZATION REPORT NUMBER(S)		
6a. NAME OF PERFORMING ORGANIZATION HYDROLOGIC ENGINEERING CENTER USA CORPS OF ENGINEERS		6b. OFFICE SYMBOL (If applicable) CEWRC-HEC	7a. NAME OF MONITORING ORGANIZATION		
6c. ADDRESS (City, State, and ZIP Code) 609 SECOND STREET DAVIS CA 95616			7b. ADDRESS (City, State, and ZIP Code)		
8a. NAME OF FUNDING / SPONSORING ORGANIZATION WATER RESOURCES SUPPORT CENTER		8b. OFFICE SYMBOL (If applicable) CEWRC	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER		
8c. ADDRESS (City, State, and ZIP Code) CASEY BUILDING # 2594 FT BELVOIR VA 22060-5586			10. SOURCE OF FUNDING NUMBERS		
			PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO.
			WORK UNIT ACCESSION NO.		
11. TITLE (Include Security Classification) APPLICATION OF THE HEC PRESCRIPTIVE RESERVOIR MODEL IN THE COLUMBIA RIVER SYSTEM					
12. PERSONAL AUTHOR(S) RICHARD HAYES, MICHAEL BURNHAM, AND DAVID FORD					
13a. TYPE OF REPORT TECHNICAL PAPER		13b. TIME COVERED FROM _____ TO _____		14. DATE OF REPORT (Year, Month, Day) MAY 1993	
15. PAGE COUNT 14					
16. SUPPLEMENTARY NOTATION					
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP	SYSTEM ANALYSIS, RESERVOIR MODELING, OPERATIONS RESEARCH, NETWORK-FLOW PROGRAMMING, OPERATION STUDIES, RESERVOIR OPERATING RULES.		
19. ABSTRACT (Continue on reverse if necessary and identify by block number) This paper summarizes the interim findings of the second phase of the HEC-PRM Columbia River application. The HEC-PRM represents the Columbia system as a link-node network and uses network-flow programming to optimize, in time and space, flow and storage in the system. The representation of operational goals in HEC-PRM is accomplished through flow, storage, and energy economic penalty functions. Operational purposes represented by penalty functions included hydropower, water supply, flood control, navigation, recreation, and anadromous fish. The application was based on fifty year period-of-record with a monthly time interval. The HEC data storage system, HEC-DSS, was utilized extensively for data management and analysis of results.					
20. DISTRIBUTION / AVAILABILITY OF ABSTRACT <input type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT. <input type="checkbox"/> DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION		
22a. NAME OF RESPONSIBLE INDIVIDUAL RICHARD J. HAYES, Hydraulic Engineer			22b. TELEPHONE (Include Area Code) (916) 756-1104		22c. OFFICE SYMBOL CEWRC-HEC